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## New Tests for Cointegration in Heterogeneous Panels

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#### Abstract

This paper makes the following contributions to the existing literature on panel cointegration. First, two new tests based on the principle of weighted symmetric estimation are proposed for panel cointegration testing. Second, the asymptotic distributions of these new tests are examined, and these are shown to be well defined Weiner processes that are free of nuisance parameters. Third, the size and power properties of the proposed tests are studied with a Monte Carlo simulation, and their properties are found to be superior to those of the existing tests across a range of environments. *Keywords*: Panel coingtegration test; heterogeneous panel data

JEL classification: C12; C15; C22; C23

## 1 Introduction

Panel data is commonly used in empirical research today by economists. Following the study of unit root tests in panels, research examining the properties of non-stationary time series in panel form is becoming more and more developed. Kao (1997) and Pedroni (1997) proposed the original tests for cointegration in panels under the null of no cointegration, and these tests are the most commonly used tests in empirical work. The Kao (1997) test is used for homogeneous panels. Pedroni(1997) gives two sets of statistics: the first set is for testing cointegration in homogeneous panels and the second set of statistics is for testing cointegration in heterogeneous panels.

McCoskey and Kao (1998) proposed the use of the average of the Augmented Dickey-Fuller (ADF) statistics over cross-sections based on Im *et al.*(1997) to test the hypothesis of no cointegration in heterogeneous panels.

In this paper, based on the idea of Maddala and Wu (1999) of using the Fisher test and the previously known weighted symmetric (WS) estimation, we proposed three new tests: the average weighted symmetric (AWS) test, the Fisher-ADF (FADF) test and the Fisher weighted symmetric (FWS) test, for testing cointegration in heterogeneous panels with the null hypothesis of no cointegration.

Although weighted symmetric estimation was first introduced by Park and Fuller (1993), this estimation method has not been used by economists doing empirical work in time series. Weighted symmetric estimation usually brings better results compared with the Dickey-Fuller (DF) and ADF estimations, the most commonly used estimation methods in time series. It was shown by Pantula *et al.* (1994) that the test using weighted symmetric estimation is the most powerful test for testing unit roots in a single time series. Hoang and McNown (2006) found that weighted symmetric estimation also dominates the other estimation methods in testing unit roots in panel data in terms of test power. In testing cointegration in hetero-

## 2 Current Tests for Cointegration in Panel Data

## 2.1 Testing for Cointegration in Homogeneous Panels

Chihwa Kao (1997) considered the following system of cointegrated regressions in the homogeneous panels:

Let

 $x_{it} = x_{it-1} + it$  $y_{it} = y_{it-1} + v_{it}$ 

The OLS estimate of is:

$$\hat{} = \frac{N}{N} \frac{T}{t=2} \hat{U}_{it} \hat{U}_{it-1}}{N} \frac{T}{t=2} \hat{U}_{it-1}^2 \hat{U}_{it-1}^2$$

The null hypothesis that = 1 is tested by:

$$\overline{N}T(\hat{-}1) = \frac{\frac{1}{\sqrt{N}} \quad \stackrel{N}{\underset{i=1}{i=1}} \frac{1}{T} \quad \stackrel{T}{\underset{t=2}{t=2}} \hat{U}_{it-1} \quad \hat{U}_{it}}{\frac{1}{N} \quad \stackrel{N}{\underset{i=1}{i=1}} \frac{1}{T^2} \quad \stackrel{T}{\underset{t=2}{t=2}} \hat{U}_{it-1}^2}$$

The second is an Augmented-Dickey-Fuller(ADF) type test which can be calculated from:

$$\hat{u}_{it} = \hat{u}_{it-1} + \sum_{\substack{j = 1 \\ j=1}}^{p} \hat{u}_{it-j} + e_{itp}$$
(3)

where p is chosen so that the residuals  $e_{itp}$  are serially uncorrelated. The ADF test statistic here is the usual t-statistic with = 1 in the ADF equation.

The following specification of null and alternative hypotheses is used:  $H_0$ : = 1,  $H_1$ : < 1.

Kao proposes four DF-type statistics and an ADF statistic. The first two DF statistics are based on assuming strict exogeneity of the regressors with respect to the errors in the equation, while the remaining two DF statistics allow for endogeneity of the regressors. The DF statistic, which allows for endogeneity, and the ADF statistic involve deriving some nuisance parameters from the long-run conditional valloareprop17Tho7(o)-297(-378(o)1(11t)]TJF351(121)

## 2.2 Testing for Cointegration in Heterogeneous Panels

#### 2.2.1 Pedroni (1997)

Pedroni (1997) considers the following model for heterogeneous panel data

$$y_{it} = {}_{i} + x_{it} {}_{i} + u_{it}$$
 (4)  
(*i* = 1,..., *N*, *t* = 1,..., *T*)

For the processes:

$$x_{it} = x_{it-1} + it$$
$$y_{it} = y_{it-1} + V_{it}$$

where *i* are individual constant terms, *i* is the slope parameter for the cross-section i of the panel, *it*,  $v_{it}$  are stationary disturbance terms and so  $y_{it}$  and  $x_{it}$  are integrated processes of order 1 for all *i* 

The zero mean vector  $it = (v_{it}, it)'$  is assumed to satisfy

$$\frac{1}{\overline{T}}_{t=1}^{[Tr]} it = B_i(i)$$

for each cross-section *i* as T - i, where  $B_i(i)$  is a vector of Brownian motion on the interval r = [0, 1] with asymptotic covariance *i*. The asymptotic covariance matrix *i* is given by:

$$i = \lim_{T \to \infty} E \quad \frac{1}{T} \begin{pmatrix} T & t \\ t=1 \end{pmatrix} \begin{pmatrix} T & t \\ t=1 \end{pmatrix}$$

and can be decomposed as:

i = i + i + i

from the separate regression for each panel member (4) and compute the lower triangular decomposition of the  $\hat{}_i$  given in (5). Finally, run the following regression for each member of the panel:

$$\hat{u}_{it} = \hat{i}\hat{u}_{it-1} + \hat{e}_{it} \tag{7}$$

and construct the group mean statistics for the null of no cointegration in heterogeneous panels as:

$$\tilde{Z}_{NT-1} = \prod_{i=1}^{N} \frac{\prod_{t=1}^{T} (\hat{u}_{it-1} \quad \hat{u}_{it} - \hat{i})}{\prod_{t=1}^{T} \hat{u}_{it-1}^{2}}$$
(8)

$$\tilde{Z}_{t_{NT}} = \prod_{i=1}^{N} \frac{\prod_{t=1}^{T} (\hat{u}_{it-1} \quad \hat{u}_{it} - \hat{i})}{\prod_{t=1}^{T} \frac{1}{\hat{L}_{11i}^2} \hat{u}_{it-1}^2}$$
(9)

Where  $\hat{L}_{11i} = (\hat{1}_{11i} - \hat{2}_{21i}/\hat{2}_{22i})^{1/2}$ .  $\hat{i}_i$  is estimated as in (5).  $\hat{i}_i = \frac{1}{2}(\hat{i}_i - \hat{s}_i^2)$ , for which,  $\hat{s}_i^2$  is the contemporaneous variance of  $\hat{e}_{it}$  and  $\hat{i}_i^2$  is the long-run variance of  $\hat{e}_{it}$ , they are consistently estimated by:

$$\hat{S}_{i}^{2} = \frac{1}{T} \int_{t=1}^{T} \hat{e}_{it}^{2}$$
(10)

$$\hat{f}_{i}^{2} = \frac{1}{T} \int_{t=1}^{T} \hat{e}_{it}^{2} + 2 \int_{s=1}^{k_{i}} 1 - \frac{s}{k_{i}+1} \int_{t=s+1}^{T} \hat{e}_{it} \hat{e}_{it-s}$$
(11)

Pedroni showed that under the null of no cointegration ( $_{i} = 1$  i = 1, 2, ..., N in the equation  $\hat{u}_{it} = \hat{u}_{it-1} + \hat{e}_{it}$ ).  $\frac{\tau}{\sqrt{N}}\tilde{Z}_{N\tau-1}$  and  $\frac{1}{\sqrt{N}}\tilde{Z}_{\hat{t}_{N\tau}}$  converge to the normal distributions with both T and N – . With the Monte-Carlo results the asymptotic distributions of these statistics can be written as:

$$\frac{T}{N}\tilde{Z}_{NT-1} + 9.05 \quad \overline{N} = -\frac{L}{N} N(0, 35.98)$$
(12)

$$\frac{1}{\overline{N}}\tilde{Z}_{\hat{t}_{NT}} + 2.03 \quad \overline{N} - N(0, 0.66)$$
(13)

One can use these results to test the hypothesis of no cointegration in every cross-section of a panel.

### 2.2.2 McCoskey and Kao (1998)

McCoskey and Kao (1998) propose the average Augmented Dickey-Fuller (ADF) test for varying slopes and varying intercepts across all the members of the panel. They consider the model:

$$y_{it} = i + x_{it} + u_{it}$$
 (14)

(i = 1)

The null hypothesis is

that WS estimation produces test statistic with greater power than those based on simple least squares. In this section, we give the limiting distribution of the WS estimator and the WS pivotal statistics when using WS estimation in testing unit root and cointegration in a single time series.

### 3.1 Alternative Representations of an Autogregressive Process

The following theorem is taken from Fuller (1996).

#### Theorem 3.0

Let  $\{X_t\}$  be a time series defined on the integers with  $E\{X_t^2\} < K$  for all t. Suppose  $X_t$  satisfies

$$X_{t} + \int_{j=1}^{p} X_{t-j} = e_{j}$$
$$t = 0, \pm 1, \pm 2, \dots$$

where  $\{e_t\}$ ,  $t = 0, \pm 1, \pm 2, ...$ , is a sequence of uncorrelated (0, 2) random variables. Let  $m_1, m_2, ..., m_p$  be the roots of the characteristic equation

$$m^p + \int_{j=1}^p m^{p-j} = 0$$

and assume  $|m_i| < 1$ , i = 1, 2, ..., p. Then  $X_t$  is covariance stationary. Furthermore,  $X_t$  is given as a limit in mean square by

$$X_t = \int_{j=0}^{\infty} W_j e_{t-j}$$

where  $\{w_j\}_{j=0}^{\infty}$  is the unique solution of the homogeneous di erence equation  $w_j + w_{j-1} + \dots + pw_{j-p} = 0$ ,  $j = p, p + 1, \dots$ , subject to the boundary conditions  $w_0 = 0$  and  $w_j + w_{j-1} + \dots + pw_{j-p} = 0$ ,  $j = 1, 2, \dots, p - 1$ 

**Proof:** See Fuller (1996, p.59).

We now know that a time series satisfying a pth order di erence has a representations as an infinite moving average.

#### **Proposition 3.1**

If the time series  $\{X_t\}$ ,  $t = 0, \pm 1, \pm 2, ...,$  with zero mean satisfies

$$X_t + {}_1X_{t-1} + {}_2X_{t-2} + \dots + {}_pX_{t-p} = e_t$$

where  $\{e_t\}$  is a sequence of uncorrelated (0, 2) random variables, and the roots  $m_1, m_2, ..., m_p$  of the characteristic equation

$$\mathcal{M}^{p} + {}^{p} + {}^{p} + {}^{p} + {}^{2993} \mathcal{M}_{+} \mathcal{I}_{+} \mathcal{I}_{-2983} \mathcal{I}_{+} \mathcal{I$$

gressive time series

Run the regression (30) and get the residual  $\hat{u}_t$ . We apply the weighted symmetric unit root test on  $\hat{u}_t$ . The estimation equation is

$$\hat{u}_t = \hat{u}_{t-1} + e_t, \ t = 1, 2, \dots, T \tag{31}$$

The weighted symmetric estimator of is the one to minimize

$$Q = \int_{t=2}^{T} W_t (\hat{u}_t - \hat{u}_{t-1})^2 + \int_{t=1}^{T-1} (1 - W_{t+1}) (= \hat{1})^{T-1} (1 - W_{t+1}$$

$$B_{v} = \int_{0}^{1} V(r) dr = 2V(1) \int_{0}^{1} V(r) dr + [V(1)]^{2}$$

$$B_{w} = \int_{0}^{1} W(r) dr = 2W(1) \int_{0}^{1} W(r) dr + [W(1)]^{2}$$

$$C = \int_{0}^{1} [V(r)]^{2} dr - \int_{0}^{1} V(r) dr = 2 \int_{0}^{2} \int_{0}^{1} [W(r)]^{2} dr - \int_{0}^{1} W(r) dr = 2$$

$$D = \int_{0}^{1} V(r) dr = 2 \int_{0}^{2} V(r) dr = 2 \int_{0}^{1} V(r) dr = 1 \int_{0}^{1} W(r) dr$$

$$= \frac{\int_{0}^{1} V(r) W(r) dr - \int_{0}^{1} V(r) dr = 1 \int_{0}^{1} W(r) dr}{\int_{0}^{1} [W(r)]^{2} dr - \int_{0}^{1} W(r) dr}$$

V(r) and W(r) are the standard Wiener processes on [0,1].

**Proof:** See Appendix

The limiting distribution of WS test statistics for cointegration in single set of time series is free of nuisance parameters and depends only on the number of regressors. A simulation can provide the values of moments of the distribution which can be used to test for cointegration in heterogeneous panels.

# 4 New Tests for Cointegration in Heterogeneous Panels

In this section, new tests are presented that are based on the idea of average test statistics for each member of a panel, used in Im *et al.*(2003) to test for unit roots in panels, and Fisher's approach to combine p-values from individual test in each cross-section which is introduced in Maddala and Wu (1999). We introduce the use of three new tests for testing cointegration in heterogeneous panels.

First we briefly recall the Im et al. and Fisher tests. The Im et al. statistic is based on

the average individual Dickey-Fuller unit root tests as

$$t_{IPS} = - \overline{N(\overline{t} - E[t_i/_i = 1])}$$

Obtain the WS estimator of (37) and then compute the WS t-statistics  $t_{IWS}$  for (37) in each cross-section i. Finally, compute the WS panel statistic

$$\overline{t}_{WS} = \frac{1}{N} \prod_{i=1}^{N} t_{iWS}$$

Define  $E[t_{iWS}] = \mu_{WS}$ , and  $Var[t_{iWS}] = \frac{2}{WS}$ . Then the central limit theorem can be applied to give:

$$\overline{N}\frac{(\overline{t}_{WS}-\mu_{WS})}{WS} \stackrel{L}{\longrightarrow} N(0,1)$$

In the case that  $\{e_{it}\}$  are correlated, instead of using (37), we can use the augmented equation to account for the correlation between  $\{e_t\}$ 

.

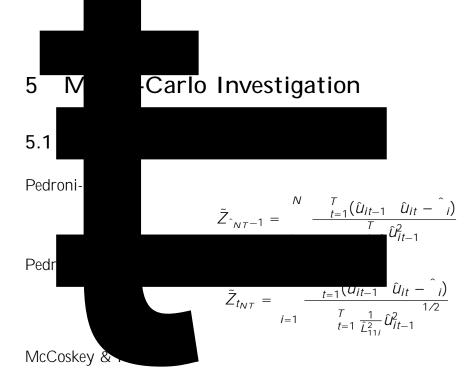
and get the residual  $\hat{u}_{it}$ . The estimation equation is

$$\hat{u}_{it} = \hat{u}_{it-1} + \int_{j=1}^{p} \hat{u}_{it-j} + e_{itp}$$
(40)

The FADF test requires deriving the distribution of the Dickey-Fuller t-statistic, for which the simulated values were generated for di erent *T* and *p*. Then the p-values  $_{iadF}$  for each ADF t-statistic could be derived. Consequently, the panel FADF statistic  $P_{FADF}$  is calculated as:  $P_{FADF} = -2 \sum_{i=1}^{N} log_{e \ iadF} = \frac{2}{2N}$ . For the critical values of the FADF statistic we use the  $^{2}$  table.

### 4.3 Fisher Weighted Symmetric Test (FWS)

The FWS test is the same as the FADF test except here we use the WS estimation procedure for each cross section rather than the ADF estimation procedure. The FWS test is based on the proposition 3.5 that the WS t-statistics for testing cointegration in single time series will converge to a function of standard Wiener processes with no nuisance parameters. The FWS test also requires deriving the distribution of the WS t-statistic, for which simulations were generated and the p-values *iws* for each WS t-statistic could be computed. The panel FWS statistic  $P_{FWS}$  is calculated as:  $P_{FWS} = -2 \sum_{i=1}^{N} log_{e iws} = \frac{2}{2N}$ . For the critical values of FWS statistics  $P_{FWS}$  for each N, we use the -2 table. The advantage of the Fisher test is that it does not require a balanced panel as the average test does.



## 5.2 Data Generation Processes

The DGP for all six tests based on the null hypothesis of no cointegration is as follows:

$$y_{it} = {}_{i} + {}_{i}x_{it} + U_{it}$$
 (41)  
(*i* = 1, ..., *N*, *t* = 1, ..., *T*)

and

$$U_{it} = U_{it-1} + V_{it}$$

It is also assumed that

$$X_{it} = X_{it-1} + it$$

where  $_{it} N(0, _i^2)$ , so we have that  $y_{it}$  and  $x_{it}$  are random walks, so they are cointegrated series if // < 1 but are not cointegrated, implying (41) is a spurious regression, if = 1. The size of the tests are investigated under the null hypothesis = 1. For studying the power of tests we set = 0.9. The autocorrelation in  $v_{it}$  takes the form of moving average component as

$$V_{it} = V_{it}^* + V_{it-1}^*$$

where  $v_{it}^* = N(0, 1)$  and

$$\begin{array}{ccccccc} v_{it}^* & 0 & 1 & i \\ & N & , & \\ it & 0 & i & \frac{2}{i} \end{array}$$

*i*, *i* and *i* are generated using the uniform distribution as: *i* U[0, 10], *j* U[0, 2] and *j* U[0.5, 1.5]. *i*, *i* and *j* are generated once and fixed in all replications. The choice of N and T for the experiment is :  $N = \{5, 10, 25, 50\}$  and  $T = \{10, 25, 50, 100\}$ .

We examine four groups of DGPs by controlling the values of and *i* 

(1)-There is no endogeneity between  $x_{it}$  and  $u_{it}$  and no autocorrelation in  $v_{it}$ : = 0 and i = 0

(2)-There is endogeneity between  $x_{it}$  and  $u_{it}$  but no autocorrelation in  $v_{it}$ : = 0.5 and i = 0

(3)-There is no endogeneity between  $x_{it}$  and  $u_{it}$  but autocorrelation in  $v_{it}$ : = 0 and U[-0.4, 0.4]

(4)-There is both endogeneity between  $x_{it}$  and  $u_{it}$  and autocorrelation in  $v_{it}$ : = 0.5 and U[-0.4, 0.4]

To reduce the e ect of initial conditions, T+50 observations are generated and the first 50 observations are eliminated, using only last T observations. The number of replications is set to 3,000 for computing the empirical size and power of all five tests. The size and power of tests are computed at the 5% nominal level.

The data generating processes here is adopted similarly to the DGP used in the McCoskey and Kao (1998) paper.

#### 5.3 Size and Power of Tests

The results of the simulation experiments are reported in Tables 2-5. In all cases, 3000 trials are used to examine the size and power properties. Table 2<sup>1</sup> presents the first set of experiments when there is no endogeneity between  $x_{it}$  and  $u_{it}$  and also no autocorrelation in  $v_{it}$ . The critical value of the 5% significance level is used to calculate the size and power of the tests. The Pedroni-t test has a strong size distortion, growing large when T or N increases. This size distortion makes the test impractical with large probability of a type I error. The Pedroni-t test has a little size distortion also, the size of this test is slightly under the significance level of 5% when T is small. It becomes larger when T increases, so at

<sup>&</sup>lt;sup>1</sup>All simulations are performed using Matlab 7.0 on a 3.44 GHz, 2GB Ram PC. The programs are available upon requested.

T=100, the size is around 10%. It is noted that the size does not change when N increases. The size of the McCoskey and Kao test is under 5% also, and it is smaller when both N and T are larger, and it decreases faster when N increases compared to when T increases. Although the Pedroni- and McCoskey and Kao tests are undersized, they are still acceptable, as it would lower the chance one could commit a type I error in testing a hypothesis. For all three proposed tests, AWS, FADF and FWS, the size is good, mostly lying between 4% and 6%. In terms of the power of tests, all five tests have good power when T is large. The power increases when N increases, but the speed of the increase is slower compared to the case when T increases. Overall the two tests AWS and FWS have more power which dominates those of other four tests, especially when T is less than 50. For instance, when N=25 and T=25, the powers of AWS and FWS are 50% and 35% compared to the power of other four tests. (14% (Pedroni-t), 10% (Pedroni-), 6% (McCoskey & Kao) and 17% (FADF)). When both N and T are large, AWS and FWS are still the most powerful tests. In the first set of experiments all three tests AWS, FADF, FWS have good size and the tests AWS and FWS have the highest power. The FADF test does not have as good power as the AWS and FWS tests when N is small, but when N is larger than 25 its power is also good. In this case the Pedroni-t test should not be used in practice because of serious size distortion. In both size and power the performances of AWS and FWS dominate the other tests. The AWS test has slightly more power than the FWS, so in this case AWS is the best choice. However, it should be noted that AWS is only for balanced panels, so in the case when we have an unbalanced panel, the FWS would be of first choice.

Table 3 reports the size and power of tests when there is endogeneity between  $x_{it}$  and  $u_{it}$  but there is no autocorrelation in  $v_{it}$ . The Pedroni-t test has size distortion, most of them are close to zero, unlike the environment of table 2. Here the correction for endogeneity of the t-statistics of the Pedroni-t test through the term  $L_{11i}^{-2}$  helps to reduce the size if endogeneity really exists. The fact that the size is almost zero is acceptable in practice because it will help

to reduce the chance of type I error. The size of the Pedroni- test tends to under 5% when T is small and become a little over 5% when T is larger than 50, and when N=50, T=100, it gets to a maximum of 13%. The McCoskey & Kao test's size is a bit under the nominal size of 5%, and it does not change much when N or T changes. All three new tests, AWS, FADF, FWS, have good size, all falling between 4% to 6%. The power of the Pedroni-t test is low when T and N are small, especially when T is less than 50, and the power decreases even when N increases. When T=100, the power increases as N increase. The cause of the low power of the Pedroni-t test is better: it is powerful when N 25 and T 50 but it is poor when N < 25 or T < 50. Again, the two test AWS and FWS are the most powerful tests. The AWS is a little more powerful than the FWS, but they both dominate other

of the correlation coe cient ; that is randomly set as ; [-0.4, 0.4]. Apparently when the correlation coe cient *i* in the moving average term is large, the correction for this in the Pedroni- test through the term *i* does not work well. The McCoskey and Kao test has a small (under-size) distortion, which is acceptable as it reduces the chance to get type I error in testing a hypothesis. For all three of the proposed tests, AWS, FWS, FADF, the size is good, lying close to the nominal size of 5% for every value of N and T. This simulation evidence confirms that the limiting distributions of all these three tests are approximated well by the standard normal and Chi-squared distributions, based on the fact that they exhibit good and stable size under di erent panel dimensions. In terms of power the Pedroni-t test perform well but because it has serious size distortion its strong power in this case is not useful. The Pedroni- test is less powerful when T 25 and has good power when T 50, but when T 50 its size is small. In general, the Pedroni- test in this case is unreliable, requiring a trade o between good power and bad size or good size and bad power. The tests with the most power are still the AWS and FWS, while the third best is FADF which is a little more powerful than the McCoskey and Kao test. Compared to table 2 and table 3, they are even more powerful in the presence of moving average correlation in  $v_{it}$ . So in this case, both Pedroni tests are unreliable, while the Mc-328(ic-he)-3046-23.24

in terms of size and power compared to the Pedroni tests and the McCoskey and Kao test, in every combination of endogeneity or moving average autocorrelation considered in this study. We propose that in practice, if the data is a balanced panel, the AWS test should be used and if the panel is unbalanced the FWS should be the first choice. The programs for these two tests are available from the author and make it easy to use in empirical work. An important extension for future study would be the e ect of cross-section correlation on testing cointegration of these tests in panels.

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р	Т	MEAN	VARIANCE
2	7	-1.1343	1.1680
2	8	-1.1953	1.1649
2	9	-1.2412	1.1263
2	10	-1.2802	1.1084
2	15	-1.4039	1.0750
2	20	-1.4700	1.0439
2	25	-1.5117	1.0154
2	30	-1.5494	0.9866
3	40	-1.5513	0.9713
3	50	-1.5784	0.9515
3	60	-1.6083	0.9398
3	70	-1.6202	0.9231
3	80	-1.6392	0.9095
3	90	-1.6454	0.9034
4	100	-1.6137	0.8966
4	150	-1.6510	0.8855
4	1	I	1

TABLE 1: Moments of t-statistics of the Weighted Symmetric Estimator in Testing Cointegration in a Single Equation

Ν	T	PEDRONI-	PEDRONI-	MCCOSKEY	AVERAGE-	FISHER-	FISHER	
		t		& KAO- <i>t<sub>ADF</sub></i>	t <sub>WS</sub>	t <sub>ADF</sub>	t <sub>WS</sub>	
				SIZ	E			
5	10	0.000	0.000	0.032	0.051	0.050	0.047	
	25	0.058	0.012	0.028	0.049	0.053	0.054	
	50	0.216	0.044	0.032	0.045	0.055	0.049	
	100	0.315	0.072	0.025	0.042	0.045	0.045	
10	10	0.000	0.000	0.013	0.048	0.040	0.045	
	25	0.066	0.010	0.016	0.047	0.042	0.050	
	50	0.268	0.044	0.021	0.044	0.043	0.038	
	100	0.463	0.093	0.025	0.053	0.052	0.050	
25	10	0.000	0.000	0.003	0.052	0.047	0.049	
	25	0.039	0.006	0.008	0.055	0.052	0.062	
	50	0.445	0.052	0.010	0.057	0.044	0.052	
	100	0.709	0.102	0.020	0.059	0.055	0.052	
50	10	0.000	0.000	0.000	0.055	0.047	0.052	
	25	0.024	0.003	0.002	0.052	0.043	0.054	
	50	0.640	0.056	0.005	0.052	0.040	0.047	
	100	0.913	0.131	0.007	0.062	0.045	0.053	
		POWER						
5	10	0.001	0.000	0.030	0.077	0.052	0.067	
	25							

TABLE 2: Size and Power of Tests for Cointegration in the Panels with Heterogeneity of the Intercepts and Slopes: (=0; =0)

N         T         PEDRONI- t         PEDRONI- biol         PEDRONI- MCCOSKEY         AVERAGE- tws         FISHER- t <sub>M/S</sub> FISHE					ercepts and Slo		; $i = 0$ )				
	N	Т	PEDRONI-	PEDRONI-	MCCOSKEY	AVERAGE-	FISHER-	FISHER-			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			t		& KAO- <i>t<sub>ADF</sub></i>	t <sub>WS</sub>	t <sub>ADF</sub>	t <sub>WS</sub>			
25         0.002         0.009         0.028         0.046         0.053         0.051           100         0.021         0.073         0.029         0.042         0.044         0.052           100         0.021         0.073         0.027         0.043         0.047         0.046           10         10         0.000         0.000         0.020         0.053         0.055         0.048           50         0.003         0.051         0.024         0.053         0.050         0.058           100         0.113         0.075         0.023         0.044         0.047         0.045           25         10         0.000         0.000         0.004         0.059         0.048         0.052           25         10         0.000         0.006         0.005         0.050         0.049         0.060           50         0.001         0.055         0.015         0.050         0.052         0.051           100         0.004         0.095         0.015         0.051         0.044         0.055           50         100         0.000         0.002         0.002         0.047         0.049         0.055											
50         0.009         0.050         0.029         0.042         0.044         0.052           100         0.021         0.073         0.027         0.043         0.047         0.046           10         10         0.000         0.000         0.020         0.053         0.055         0.048           25         0.000         0.012         0.019         0.042         0.050         0.038           100         0.013         0.075         0.023         0.046         0.047         0.045           25         10         0.000         0.004         0.059         0.048         0.052           25         0.00         0.006         0.005         0.050         0.049         0.060           50         0.001         0.055         0.015         0.050         0.052         0.051           100         0.004         0.095         0.015         0.051         0.044         0.055           50         10         0.000         0.000         0.056         0.054         0.052         0.054           50         0.000         0.002         0.022         0.047         0.499         0.555           50         0.000	5	10	0.000	0.000	0.031			0.053			
100         0.021         0.073         0.027         0.043         0.047         0.046           10         10         0.000         0.000         0.020         0.053         0.055         0.048           25         0.000         0.012         0.019         0.042         0.050         0.038           50         0.003         0.051         0.024         0.053         0.050         0.058           100         0.013         0.075         0.023         0.046         0.047         0.045           25         10         0.000         0.004         0.059         0.048         0.052           25         0.001         0.055         0.015         0.050         0.044         0.050           100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.002         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.52         0.054           100         0.010         0.126         0.015         0.054         0.056         0.051           50         0.027		25	0.002	0.009	0.028		0.053	0.051			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		50	0.009	0.050	0.029		0.044	0.052			
25         0.000         0.012         0.019         0.042         0.050         0.038           50         0.003         0.051         0.024         0.053         0.050         0.058           100         0.013         0.075         0.023         0.046         0.047         0.045           25         10         0.000         0.000         0.004         0.059         0.048         0.052           25         0.000         0.006         0.005         0.050         0.049         0.060           50         0.001         0.055         0.015         0.051         0.044         0.050           50         0.000         0.000         0.000         0.056         0.046         0.053           25         0.000         0.002         0.002         0.047         0.044         0.050           50         10         0.000         0.002         0.002         0.047         0.044         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           50         0.001         0.126         0.015         0.054         0.056         0.051           50         0.027		100	0.021	0.073	0.027	0.043	0.047	0.046			
50         0.003         0.051         0.024         0.053         0.050         0.058           100         0.013         0.075         0.023         0.046         0.047         0.045           25         10         0.000         0.004         0.059         0.048         0.052           25         0.001         0.055         0.015         0.050         0.049         0.060           50         0.001         0.055         0.015         0.051         0.044         0.050           100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.000         0.056         0.046         0.053           25         0.000         0.002         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253	10	10	0.000	0.000	0.020	0.053	0.055	0.048			
100         0.013         0.075         0.023         0.046         0.047         0.045           25         10         0.000         0.006         0.005         0.059         0.048         0.052           25         0.000         0.006         0.005         0.050         0.049         0.060           50         0.011         0.055         0.015         0.050         0.052         0.051           100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.000         0.056         0.046         0.053           25         0.000         0.002         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839		25	0.000	0.012	0.019	0.042	0.050	0.038			
25         10         0.000         0.000         0.004         0.059         0.048         0.052           25         0.000         0.006         0.005         0.050         0.049         0.060           50         0.001         0.055         0.015         0.050         0.052         0.051           100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.000         0.002         0.056         0.046         0.053           25         0.000         0.002         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.52         0.054           100         0.011         0.126         0.015         0.054         0.056         0.061           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.017         0.51         0.067           25         0.001		50	0.003	0.051	0.024	0.053	0.050	0.058			
25         0.000         0.006         0.005         0.050         0.049         0.060           50         0.001         0.055         0.015         0.050         0.052         0.051           100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.000         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.051           50         0.000         0.036         0.069         0.056         0.061           7         0.027         0.234         0.110         0.253         0.133         0.202           10         0.000         0.000         0.019         0.077         0.051         0.667           55         0.017         0.334         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000		100	0.013	0.075	0.023	0.046	0.047	0.045			
50         0.001         0.055         0.015         0.050         0.052         0.051           100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.000         0.002         0.022         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.051           50         0.000         0.038         0.0057         0.052         0.054           0.001         0.126         0.015         0.056         0.051           0.001         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153<	25	10	0.000	0.000	0.004	0.059	0.048	0.052			
100         0.004         0.095         0.015         0.051         0.044         0.050           50         10         0.000         0.000         0.002         0.047         0.049         0.055           50         0.000         0.002         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.051           POWER           5         10         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.277         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.017         0.051         0.067           25         0.001         0.355         0.433         0.151         0.087         0.127           50 <th></th> <th>25</th> <th>0.000</th> <th>0.006</th> <th>0.005</th> <th>0.050</th> <th>0.049</th> <th>0.060</th>		25	0.000	0.006	0.005	0.050	0.049	0.060			
50         10         0.000         0.000         0.002         0.002         0.046         0.053           25         0.000         0.002         0.002         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.051           POWER           5         10         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.27         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323 <t< th=""><th></th><th>50</th><th>0.001</th><th>0.055</th><th>0.015</th><th>0.050</th><th>0.052</th><th>0.051</th></t<>		50	0.001	0.055	0.015	0.050	0.052	0.051			
25         0.000         0.002         0.007         0.047         0.049         0.055           50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.051           5         10         0.000         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.001         0.017         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000		100	0.004	0.095	0.015	0.051	0.044	0.050			
50         0.000         0.058         0.008         0.057         0.052         0.054           100         0.001         0.126         0.015         0.054         0.056         0.051           POWER           5         10         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.232           250         0.000 <th>50</th> <th>10</th> <th>0.000</th> <th>0.000</th> <th>0.000</th> <th>0.056</th> <th>0.046</th> <th>0.053</th>	50	10	0.000	0.000	0.000	0.056	0.046	0.053			
100         0.001         0.126         0.015         0.054         0.056         0.051           POWER           5         10         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.232           25         0.000         0.049         0.035         0.310         0.117         0.232           25         0.000 <th></th> <th>25</th> <th>0.000</th> <th>0.002</th> <th>0.002</th> <th>0.047</th> <th>0.049</th> <th>0.055</th>		25	0.000	0.002	0.002	0.047	0.049	0.055			
Image: Power of the system         Power of the system           5         10         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998		50	0.000	0.058	0.008	0.057	0.052	0.054			
5         10         0.000         0.000         0.036         0.069         0.056         0.063           25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.232           25         0.000         0.049         0.035         0.310         0.117         0.232           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767		100	0.001	0.126	0.015	0.054	0.056	0.051			
25         0.004         0.035         0.049         0.121         0.075         0.109           50         0.027         0.234         0.110         0.253         0.133         0.202           100         0.213         0.839         0.414         0.723         0.415         0.619           10         10         0.000         0.009         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.063         0.090           25         0.000         0.049         0.035         0.310         0.117         0.232           25         0.000         0.049         0.035         0.310         0.117         0.232           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.000         0.000											
500.0270.2340.1100.2530.1330.2021000.2130.8390.4140.7230.4150.61910100.0000.0000.0190.0770.0510.067250.0010.0350.0430.1510.0870.127500.0170.3900.1530.4510.1900.3231000.3630.9830.7110.9540.6880.88325100.0000.0070.1170.0630.090250.0000.0490.0350.3100.1170.232500.0080.7670.3030.8310.3650.6291000.7021.0000.9851.0000.9700.99850100.0000.0010.1370.0620.09850100.0020.9670.5100.9860.6090.892	5	10	0.000	0.000	0.036	0.069	0.056	0.063			
1000.2130.8390.4140.7230.4150.61910100.0000.0000.0190.0770.0510.067250.0010.0350.0430.1510.0870.127500.0170.3900.1530.4510.1900.3231000.3630.9830.7110.9540.6880.88325100.0000.0070.1170.0630.090250.0000.0490.0350.3100.1170.232500.0080.7670.3030.8310.3650.6291000.7021.0000.9851.0000.9700.99850100.0000.0010.1370.0620.09850100.0020.9670.5100.9860.6090.892		25	0.004	0.035	0.049	0.121	0.075	0.109			
10         10         0.000         0.000         0.019         0.077         0.051         0.067           25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.063         0.090           25         0.000         0.000         0.007         0.117         0.063         0.090           25         0.000         0.000         0.007         0.117         0.063         0.090           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           25         0.000         0.081		50	0.027	0.234	0.110	0.253	0.133	0.202			
25         0.001         0.035         0.043         0.151         0.087         0.127           50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.063         0.090           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           50         10         0.000         0.001         0.137         0.062         0.098           25         0.000         0.081         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		100	0.213	0.839	0.414	0.723	0.415	0.619			
50         0.017         0.390         0.153         0.451         0.190         0.323           100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.063         0.090           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           50         10         0.000         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892	10	10	0.000	0.000	0.019	0.077	0.051	0.067			
100         0.363         0.983         0.711         0.954         0.688         0.883           25         10         0.000         0.007         0.117         0.063         0.090           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           50         10         0.000         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		25	0.001	0.035	0.043	0.151	0.087	0.127			
25         10         0.000         0.000         0.007         0.117         0.063         0.090           25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           50         25         0.000         0.081         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		50	0.017	0.390	0.153	0.451	0.190	0.323			
25         0.000         0.049         0.035         0.310         0.117         0.232           50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           50         10         0.000         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		100	0.363	0.983	0.711	0.954	0.688	0.883			
50         0.008         0.767         0.303         0.831         0.365         0.629           100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           25         0.000         0.081         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892	25	10	0.000	0.000	0.007	0.117	0.063	0.090			
100         0.702         1.000         0.985         1.000         0.970         0.998           50         10         0.000         0.001         0.137         0.062         0.098           25         0.000         0.081         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		25	0.000	0.049	0.035	0.310	0.117	0.232			
50         10         0.000         0.000         0.001         0.137         0.062         0.098           25         0.000         0.081         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		50	0.008	0.767	0.303	0.831	0.365	0.629			
25         0.000         0.081         0.032         0.521         0.174         0.358           50         0.002         0.967         0.510         0.986         0.609         0.892		100	0.702	1.000	0.985	1.000	0.970	0.998			
50 0.002 0.967 0.510 0.986 0.609 0.892	50	10	0.000	0.000	0.001	0.137	0.062	0.098			
50 0.002 0.967 0.510 0.986 0.609 0.892		25	0.000	0.081	0.032	0.521	0.174	0.358			
100 0.944 1.000 1.000 1.000 0.999 1.000			0.002	0.967	0.510	0.986	0.609	0.892			
		100	0.944	1.000	1.000	1.000	0.999	1.000			

TABLE 3: Size and Power of Tests for Cointegration in the Panels with Heterogeneity of the Intercepts and Slopes: (=0.5; =0)

NOTES: Data Generating Processes for all six tests based on the null hypothesis of no cointegration as following:  $y_{it} = i + i x_{it} + u_{it}$  (i = 1, ..., N, t = 1, ..., T) and  $x_{it} = x_{it-1} + i t$ ;  $u_{it} = u_{it-1} + v_{it}$ ;  $v_{it} = v_{it}^* + i v_{it-1}^*$  with:

$$V_{it}^*$$
 N  $\begin{pmatrix} 0 & 1 & i \\ 0 & j & 2 \\ i & 0 & j & i \\ 0 & j & 0 \end{pmatrix}$ 

where  $v_{it}^* = N(0, 1)$ ,  $it = N(0, \frac{2}{i})$ . i, i and i are generated using the uniform distribution as:

Ν	Т	PEDRONI-	PEDRONI-	MCCOSKEY	AVERAGE-	FISHER-	FISHER
		t		& KAO- <i>t<sub>ADF</sub></i>	t <sub>WS</sub>	t <sub>ADF</sub>	t <sub>WS</sub>
				SIZE	-		
5	10	0.001	0.000	0.035	0.057	0.054	0.053
	25	0.090	0.077	0.029	0.055	0.057	0.066
	50	0.342	0.053	0.026	0.043	0.047	0.048
	100	0.625	0.176	0.029	0.047	0.054	0.054
10	10	0.000	0.000	0.016	0.054	0.051	0.049
	25	0.154	0.025	0.020	0.059	0.056	0.059
	50	0.435	0.153	0.022	0.052	0.048	0.055
	100	0.802	0.273	0.024	0.049	0.055	0.052
25	10	0.000	0.000	0.004	0.067	0.050	0.056
	25	0.264	0.017	0.011	0.052	0.055	0.055
	50	0.848	0.070	0.013	0.049	0.044	0.048
	100	0.973	0.075	0.020	0.053	0.051	0.049
50	10	0.000	0.000	0.001	0.048	0.040	0.047
	25	0.376	0.030	0.003	0.060	0.056	0.068
	50	0.963	0.369	0.010	0.059	0.059	0.056
	100						

TABLE 4: Size and Power of Tests for Cointegration in the Panels with Heterogeneity of the Intercepts and Slopes: (=0; U[-0.4, 0.4])

N T PE					
	DRONI- PEDROI	NI- MCCOSKEY	AVERAGE-	FISHER-	FISHER-
		& KAO- <i>t<sub>ADF</sub></i>	t <sub>WS</sub>	t <sub>ADF</sub>	t <sub>WS</sub>

#### TABLE 5: Size and Power of Tests for Cointegration in the Panels with Heterogeneity of the Intercepts and Slopes: (=0.5; = U[-0.4, 0.4])

#### APPENDIX

Proof of Proposition 3.1:

$$X_t + {}_1X_{t-1} + {}_2X_{t-2} + \dots + {}_pX_{t-p} = e_t$$

Multiply both side by  $X_{t-h}$ 

$$X_{t-h}X_{t} + {}_{1}X_{t-h}X_{t-1} + \dots + {}_{p}X_{t-h}X_{t-p} = X_{t-h}e_{t}$$

 $E[X_{t-h}X_t] + {}_1E[X_{t-h}X_{t-1}] + \dots + {}_pE[X_{t-h}X_{t-p}] = E[X_{t-h}e_t]$ 

 $(h) + (h-1) + ... + (h-p) = E[X_{t-h}e_t]$ 

with  $(h - p) = E[X_{t-h}X_{t-p}]$  and h = 1, 2, ...

From the theorem 3.0 we have that  $X_{t-h}$  can be expressed as a weighted average if  $e_{t-h}$  and previous e's then  $X_{t-h}$  and  $e_t$  are uncorrelated  $-Cov(X_{t-h}, e_t) = E[X_{t-h}e_t] = 0$  with h = 1, 2, ... If h = 0 then

$$X_t = e_t + W_1 e_{t-1} + W_2 e_{t-2} + \dots + \dots$$

\_

$$E[X_t e_t] = E[e_t^2] + w_1 E[e_t e_{t-1}] + w_2 E[e_t e_{t-2}] + \dots + \dots = E[e_t^2] = 2$$

So we have

$$(h) + {}_{1}(h-1) + \dots + {}_{p}(h-p) = {\begin{array}{c} 0 & h = 1, 2, \dots \\ {}_{2} & h = 0 \end{array}}$$
(42)

note that, from the theorem 3.0,  $\{X_t\}$  is a covariance stationary series, then:

$$(h) = E[X_{t-h}X_t] = E[X_{t+h}X_t] = (-h)$$

and

$$E[X_{t-h}X_t] = E[X_{t+h}X_t]$$
$$E[X_{t-h}X_{t-1}] = E[X_{t+h}X_{t+1}]$$
$$\vdots$$
$$E[X_{t-h}X_{t-\rho}] = E[X_{t+h}X_{t+\rho}]$$

adding up and combine to (42)

$$E[X_{t+h}(X_t + {}_1X_{t+1} + {}_2X_{t+2} + \dots + {}_pX_{t+p})] = \begin{pmatrix} 0 & h = 1, 2, \dots \\ 2 & h = 0 \end{pmatrix}$$

or

$$E[X_{t+h}v_t] = \begin{pmatrix} 0 & h = 1, 2, \dots \\ 2 & h = 0 \end{pmatrix}$$
(43)

To prove the proposition, we need to prove:  $\{v_t\}$  is an un correlated (0, 2) random variables, this means:  $E(v_t) = 0$ ;  $E[v_t^2] = {}^2$  and  $E[v_{t+j}v_t] = 0$ ; j = 1, 2, ...

$$E(V_t) = E[X_t + {}_{1}X_{t+1} + ... + {}_{p}X_{t+p}] = E[X_t] + {}_{1}E[X_{t+1}] + ... + {}_{p}E[X_{t+p}]) = 0$$

remember that  $X_t = e_t + w_1 e_{t-1} + ... + ...$  then  $E[X_t] = E[e_t] + w_1 E[e_{t-1}] + ... + ... = 0$ 

$$E[v_t^2] = E[(X_t + {}_1X_{t+1} + ... + {}_pX_{t+p})v_t] = E[X_tv_t + {}_1X_{t+1}v_t + ... + {}_pX_{t+p}v_t] =$$
  
=  $E[X_tv_t] + {}_1E[X_{t+1}v_t] + ... + {}_pE[X_{t+p}v_t] = {}^2$ 

because of (43)

$$E[v_{t+j}v_t] = E[v_t(X_{t+j} + {}_1X_{t+j+1} + ... + {}_pX_{t+j+p})] =$$
$$= e[X_{t+j}v_t] + {}_1E[X_{t+j+1}v_t] + ... + {}_pE[X_{t+j+p}v_t] = 0$$

with j = 1, 2, ... because of (43)

Proof of Proposition 3.2:

Weighed symmetric estimator of in (16) is a ^ which minimizes:

$$Q = \sum_{t=2}^{T} W_t (y_t - y_{t-1})^2 + \sum_{t=1}^{T-1} (1 - W_{t+1}) (y_t - y_{t+1})^2$$

$$Q = \int_{t=2}^{T} \left[ (\overline{W_t}) y_t - (\overline{W_t}) y_{t-1} \right]^2 + \int_{t=1}^{T-1} (\overline{1 - W_{t+1}}) y_t - (\overline{1 - W_{t+1}}) y_{t+1}^2$$
(44)

$$W_2$$
)  $y_1$  ( $W_2$ )

if we denote:  $X = \begin{pmatrix} (\overline{W_2})y_1 & (\overline{W_2})y_2 \\ \vdots & \vdots \\ (\overline{W_T})y_{T-1} & ; Y = \begin{pmatrix} (\overline{W_T})y_T \\ (\overline{1-W_2})y_2 & \vdots \\ (\overline{1-W_T})y_T & (\overline{1-W_T})y_{T-1} \\ \vdots \\ (\overline{1-W_T})y_T & (\overline{1-W_T})y_{T-1} \end{pmatrix}$ 

and estimate (44) by

normal OLS method, we get

$$\hat{x} = [X X]^{-1} X' Y = \frac{T_{t=2} W_t (y_t y_{t-1}) + T_{t=1}^{-1} y_t y_{t+1} - T_{t=1}^{-1} W_{t+1} (y_t y_{t+1})}{T_{t=2} W_t y_{t-1}^2 + T_{t=1}^{-1} y_{t+1}^2 - T_{t=1}^{-1} W_{t+1} y_{t+1}^2}$$

finally:

$$T(^{-}-1) - \frac{\frac{1}{2}[W^{2}(1) - 1] - \frac{1}{0}[W(r)]^{2}dr}{\frac{1}{0}[W(r)]^{2}dr} = \frac{\frac{1}{2}[K^{2} - 1] - G}{G}$$

with K = W(1) and  $G = {}_{0}^{1} [W(r)]^{2} dr$ <u> $t_{0}^{*}$  distribution:</u>

$$\text{ii) } T^{-1}(y_T - \overline{y})^2 = T^{-1}(y_T^2 - 2\overline{y}y_T + (\overline{y})^2) = T^{-1} y_T^2 - 2y_T(T^{-1} \int_{t=1}^T y_t) + T^{-2}(\int_{t=1}^T y_t)^2 =$$

$$= T^{-1} y_T^2 - 2y_T T^{-1}(\int_{t=1}^T y_{t-1} + y_T) + T^{-2}(\int_{t=1}^T y_{t-1} + y_T)^2 =$$

$$= \frac{y_T}{\overline{T}} \int_{t=1}^2 -2 \frac{y_T}{\overline{T}} - \frac{1}{\overline{T}}$$

SO,

Numerator = 
$$(y_T - \overline{y})^2 - \int_{t=2}^{T} y_{t-t} + \overline{y} \int_{t=2}^{T} t - \frac{1}{T} \int_{t=1}^{T} (y_t - \overline{y})^2$$

and

$$\frac{1}{T}(numerator) = \frac{1}{T}(y_T - \overline{y})^2 - \frac{1}{T}\int_{t=2}^{T}y_{t-t} + \overline{y}_{t-1} - \frac{1}{T^2}\int_{t=1}^{T}(y_t - \overline{y})^2 - \frac{L}{t} \text{ follow lemma 1}$$
$$-\frac{L}{T^2}(H^2 - 2KH + K^2) - \frac{1}{2}[K^2 - 1] + 1 + KH - (G - H^2) = \frac{1}{2}[K^2 - 1] - G - KH + 2H^2$$
$$\frac{1}{T^2}(denominator) = \frac{1}{T^2}\int_{t=2}^{T-1}(y_t - \overline{y})^2 + \frac{1}{T}\int_{t=1}^{T}\frac{1}{T^2}\int_{t=1}^{T}(y_t - \overline{y})^2 - \frac{L}{t} \text{ follow lemma 1} - \frac{L}{T}(G - H^2)$$

## $(^- - 1)$ distribution:

$$(^{-}-1) = \frac{\int_{t=2}^{T} \hat{u}_t \hat{u}_{t-1} - \int_{t=2}^{T-1} \hat{u}_t^2 - \frac{1}{T} \int_{t=1}^{T} \hat{u}_t^2}{\int_{t=2}^{T-1} \hat{u}_t^2 + \frac{1}{T} \int_{t=1}^{T} \hat{u}_t^2}$$

we have

$$- \sum_{t=2}^{T} \hat{u}_{t} \hat{u}_{t-1} = \frac{1}{2} \sum_{t=2}^{T} \hat{u}_{t}^{2} - 2 \sum_{t=2}^{T} \hat{u}_{t} \hat{u}_{t-1} + \sum_{t=2}^{T} \hat{u}_{t-1}^{2}$$

then

$$Numerator = \int_{t=2}^{T} \hat{u}_{t} \hat{u}_{t-1} - \int_{t=2}^{T-1} \hat{u}_{t}^{2} - \frac{1}{T} \int_{t=1}^{T} \hat{u}_{t}^{2} =$$

$$= \frac{1}{2} \int_{t=2}^{T} \hat{u}_{t}^{2} + \frac{1}{2} \int_{t=2}^{T} \hat{u}_{t-1}^{2} - \frac{1}{2} \int_{t=2}^{T} (\hat{u}_{t} - \hat{u}_{t-1})^{2} - \int_{t=2}^{T-1} \hat{u}_{t}^{2} - \frac{1}{T} \int_{t=1}^{T} \hat{u}_{t}^{2} =$$

$$= \frac{1}{2} \hat{u}_{T}^{2} + \frac{1}{2} \hat{u}_{1}^{2} - \frac{1}{T} \int_{t=1}^{T} \hat{u}_{t}^{2} - \frac{1}{2} \int_{t=2}^{T} (\hat{u}_{t} - \hat{u}_{t-1})^{2}$$

SO

$$\frac{1}{T}(numerator) = \frac{1}{2} \quad \frac{\hat{u}_T^2}{T} + \frac{1}{2} \quad \frac{\hat{u}_1^2}{T} - \frac{1}{T^2} \int_{t=1}^T \hat{u}_t^2 - \frac{1}{2} \int_{t=2}^T (\hat{u}_t - \hat{u}_{t-1})^2$$

(a)

$$\frac{1}{T}\hat{u}_{T}^{2} = \frac{1}{T}(y_{T} - \hat{x}_{T})^{2} = \frac{1}{T}(y_{T} - \bar{y}) - \hat{x}_{T} - \bar{x}_{T}^{2}$$
$$= \frac{1}{T}(y_{T} - \bar{y})^{2} - 2\frac{1}{T}\hat{x}(x_{T} - \bar{x})(y_{T} - \bar{y}) + \frac{1}{T}\hat{x}^{2}(x_{T} - \bar{x})^{2}$$

we have

$$\frac{1}{T}(x_T - \overline{x})(y_T - \overline{y}) = \frac{1}{T} \quad x_T y_T - x_T \frac{1}{T} \quad y_t - y_T \frac{1}{T} \quad x_t + \frac{1}{T^2} \quad x_t + \frac{1}{T^2} \quad x_t \quad y_t =$$
$$= \frac{x_T}{T} \frac{y_T}{T} - \frac{x_T}{T} \quad \frac{1}{T^{3/2}} \quad y_t - \frac{y_T}{T} \quad \frac{1}{T^{3/2}} \quad x_t + \frac{1}{T^{3/2}} \quad x_t + \frac{1}{T^{3/2}} \quad x_t - \frac{1}{T^{3/2}} \quad x_t - \frac{1}{T^{3/2}} \quad x_t + \frac{1}{T^{3/2}} \quad x_t + \frac{1}{T^{3/2}} \quad x_t - \frac{1}{T^{3/2}} \quad x_t - \frac{1}{T^{3/2}} \quad x_t - \frac{1}{T^{3/2}} \quad x_t + \frac{1}{T^{3/2}} \quad x_t - \frac{1}{T^{3/$$

$$-\frac{L}{2} V(1)W(1) - W(1) \int_{0}^{1} V(r)dr - V(1) \int_{0}^{1} W(r)dr - \int_{0}^{1} W(r)dr \int_{0}^{1} V(r)dr = {}^{2}A$$

$$2\frac{1}{T}(x_T-\overline{x})(y_T-$$

SO

$$=\frac{X_{1}}{\overline{T}}\frac{y_{1}}{\overline{T}}-\frac{X_{1}}{\overline{T}}-\frac{1}{\overline{T}}\frac{1}{T^{3/2}}\int_{t=1}^{T}y_{t}-\frac{y_{1}}{\overline{T}}\frac{1}{T^{3/2}}\int_{t=1}^{T}X_{t}+\frac{1}{T^{3/2}}\int_{t=1}^{T}X_{t}-\frac{1}{T^{3/2}}\int_{t=1}^{T}y_{t}-\frac{L}{T^{3/2}}\int_{t=1}^{T}W(r)dr$$

From lemma 1:

$$\frac{1}{T}(y_1 - \overline{y})^2 \stackrel{L}{-} 2 \stackrel{2}{=} \frac{1}{V}(r)dr \frac{2}{r}$$
$$\frac{1}{T}(x_1 - \overline{x})^2 \stackrel{L}{-} 2 \stackrel{2}{=} \frac{1}{V}W(r)dr \frac{2}{r}$$

SO

$$\frac{1}{T}\hat{u}_{1}^{2} \stackrel{L}{\rightarrow} 2 = \begin{pmatrix} 1 \\ 0 \end{pmatrix} V(r)dr \stackrel{2}{+} 2 = \begin{pmatrix} 1 \\ 0 \end{pmatrix} W(r)dr \stackrel{2}{-} 2 = \begin{pmatrix} 1 \\ 0 \end{pmatrix} V(r)dr \stackrel{2}{-} 2 = \begin{pmatrix} 1 \\ 0 \end{pmatrix} V(r)dr \stackrel{2}{-} 2 = \begin{pmatrix} 1 \\ 0 \end{pmatrix} V(r)dr \stackrel{2}{-} 2 = \begin{pmatrix} 1 \\ 0 \end{pmatrix} V(r)dr = \begin{pmatrix} 2 \\$$

combine (a),(b),(c) and lemma 2, we have:

$$\frac{1}{T}(numerator) \stackrel{L}{=} \frac{1}{2} \stackrel{^{2}(B_{v} - 2 A + {}^{2}B_{w}) + \frac{1}{2} \stackrel{^{2}D}{=} - \stackrel{^{2}C}{=} -\frac{1}{2} \stackrel{^{2}(1 + {}^{2})}{\frac{1}{2} (1 + {}^{2})}$$

$$\frac{1}{T^{2}}(denominator) = \frac{1}{T^{2}} \stackrel{^{T-1}}{=} \hat{u}_{t}^{2} + \frac{1}{T} \stackrel{^{T}}{=} \hat{u}_{t}^{2} = \frac{1}{T^{2}} \stackrel{^{T}}{=} \frac{1}{T^{2}} \stackrel{^{T}}{=} \frac{1}{T^{2}} - \frac{\hat{u}_{1}^{2}}{T^{2}} - \frac{\hat{u}_{1}^{2}}{T^{2}} - \frac{1}{T^{3}} \stackrel{^{T}}{=} \hat{u}_{t}^{2} - \stackrel{^{L}}{=} \stackrel{^{2}C}{=} \frac{1}{T^{2}} \stackrel{^{T}}{=} \frac{1}{T^{2}} \stackrel{^{T}}{=} \frac{1}{T^{2}} - \frac{\hat{u}_{1}^{2}}{T^{2}} - \frac{1}{T^{3}} \stackrel{^{T}}{=} \frac{\hat{u}_{t}^{2}}{=} - \stackrel{^{2}C}{=} \frac{1}{T^{2}} \stackrel{^{T}}{=} \frac{1}{T^{2}} \stackrel{^{T}}}{=} \frac{1}{T^{2}} \stackrel{^{T}}{=}$$

f

$$T(\hat{-}1) - \frac{\frac{1}{2}(B_v - 2A + {}^2B_w) + \frac{1}{2}D - C - \frac{1}{2}(1 + {}^2)}{[C]}$$

*t*<sup>^</sup> distribution:

$$t_{\hat{}} = \hat{e} = \hat{e} = \hat{u}_{t=2}^{T-1} \hat{u}_{t}^{2} + \frac{1}{T} = \hat{u}_{t=1}^{T} \hat{u}_{t}^{2} = \hat{u}_{t}^{-1} - \frac{1}{2} \hat{u}_{t}^{2}$$

wh2 0J 0.478w 00.239m 18.450.239I S 1001-115.673-701.1647Tf8.4863.454Td[(3)]TJF511.93[( )]T

then:

$$t_{\uparrow} = \frac{T(\uparrow -1)}{\frac{1}{\frac{2}{T(\sum_{t=2}^{T-1}\hat{u}_{t}^{2} + \frac{1}{T}\sum_{t=1}^{T}\hat{u}_{t}^{2})}} - \frac{L}{\frac{1}{2}(B_{v} - 2A + \frac{2}{B_{w}}) + \frac{1}{2}D - C - \frac{1}{2}(1 + \frac{2}{2})}{[(1 + 2)C]^{1/2}}$$

where

$$A = V(1)W(1) - W(1) \int_{0}^{1} V(r)dr - V(1) \int_{0}^{1} W(r)dr - \int_{0}^{1} V(r)dr \int_{0}^{1} W(r)dr$$

$$B_{v} = \int_{0}^{1} V(r)dr^{2} - 2V(1) \int_{0}^{1} V(r)dr + [V(1)]^{2}$$

$$B_{w} = \int_{0}^{1} W(r)dr^{2} - 2W(1) \int_{0}^{1} W(r)dr + [W(1)]^{2}$$

$$C = \int_{0}^{1} [V(r)]^{2}dr - \int_{0}^{1} V(r)dr^{2} - 2 \int_{0}^{1} [W(r)]^{2}dr - \int_{0}^{1} W(r)dr^{2}$$

$$D = \int_{0}^{1} V(r)dr^{2} + 2 \int_{0}^{1} W(r)dr^{2} - 2 - 2$$